



RADC-TR-79-96 In-House Report March 1979

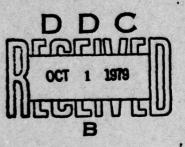


SPECKLE INTERFEROMETRY FOR A PARTIALLY COHERENT SOURCE

Ronald L. Fante

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED

DOC FILE COPY



ROME AIR DEVELOPMENT CENTER
Air Force Systems Command
Griffiss Air Force Base, New York 13441

79 10 01 159

This report has been reviewed by the RADC Information Office (OI) and is releasable to the National Technical Information Service (NTIS). At NTIS it will be releasable to the general public, including foreign nations.

RADC-TR-79-96 has been reviewed and is approved for publication.

APPROVED: Walt Rotman

WALTER ROTMAN

Chief, Antennas and RF Components Branch

APPROVED: Queanlable

ALLAN C. SCHELL

Chief, Electromagnetic Sciences Division

FOR THE COMMANDER: John P. Kluss

JOHN P. HUSS

Acting Chief, Plans Office

If your address has changed or if you wish to be removed from the RADC mailing list, or if the addressee is no longer employed by your organization, please notify RADC (EEA) Hanscom AFB MA 01731. This will assist us in maintaining a current mailing list.

Do not return this copy. Retain or destroy.

Unclassified
SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
RADC-TR-79-96	3. PECIPIENT'S CATALOG NUMBER
TITLE (and Subtitio)	5. THE OF REPORT & PERIOD COVERED
SPECKLE INTERFEROMETRY FOR A PARTIALLY COHERENT SOURCE	In-House Report
# 9 2 1	
Ronald L. Fante	8 CONTRACT OR GRANT NUMBER(s)
Deputy for Electronic Technology (RADC/EEA) Hanscom AFB	19. THOSPAN FLEMENT, PROJECT, TASK
Massachusetts 01731	23057303
Deputy for Electronic Technology (RADC/EEA)	Mar 979
Hanscom AFB Massachusetts 01731	13. NUMBER OF PAGES
14. MONITORING AGENCY NAME & ADDRESS(If different from Controlling Office)	15. SECURITY CLASS. (of this report)
160.	Unclassified
(2) - T-	154. DECLASSIFICATION DOWNGRADING
Approved for public release; distribution unlimited	
Approved for public release; distribution unlimite	m Report)
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different fro	m Report)
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different fro	DDC OCT 1 1979
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from the supplementary notes 18. Supplementary notes 19. KEY WORDS (Continue on reverse eide if necessary and identify by block number)	DDC OCT 1 1979
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different fro	DDC OCT 1 1979
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from the supplementary notes 18. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number, Turbulence Partial coherence Speckle	DDC OCT 1 1979 B
7. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from the supplementary notes 8. Supplementary notes 9. Key words (Continue on reverse side if necessary and identify by block number) Turbulence Partial coherence Speckle 10. Autract (Continue on reverse side if necessary and identify by block number) We have obtained the spatial frequency transferometry for the case when the source is partial	DDC OCT 1 1979 B fer function for speckle inter- ly coherent (spatially) and
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from the supplementary notes 18. Supplementary notes 19. Key words (Continue on reverse side if necessary and identify by block number) Turbulence Partial coherence Speckle 10. All RACT (Continue on reverse side if necessary and identify by block number) We have obtained the spatial frequency transi	fer function for speckle interly coherent (spatially) and el.

Contents

1.	INTRODUCTION	5
2.	ANALYTICAL FORMALISM	6
3.	APPROXIMATE EVALUATION OF TRANSFER FUNCTION, $H(\underline{\omega})$	10
4.	DISCUSSION	13
RE	REFERENCES	

Illustrations

1.	Geometry Assumed for the Imaging System	7
2.	Qualitative Plot of $H(\underline{\omega})$	13
3.	Qualitative Plot of $H(\underline{\omega})$ for the Case When Both $I_c \ll D$ and $I_c \ll D$	14

ACCESSION for

NTIS White Section DDC Buff Section DUNANNOUNCED DUSTIFICATION

BY DISTRIBUTION/AVAILABILITY CODES

Dist. AVAIL and/or SPECIAL

Speckle Interferometry For a Partially Coherent Source

1. INTRODUCTION

The conventional theoretical result ¹⁻⁹ for the spatial frequency spectrum of a source, as obtained using speckle interferometry ^{4,7} is based on the assumption that the source is spatially incoherent. This assumption is not restrictive when imaging distant stars, because the coherence patches are generally unresolvable by the imaging system; however, when one tries to obtain detail over sizes on the order of the spatial coherence length, the conventional theory is no longer valid, and must be modified. In this paper we will obtain the frequency transfer function for the combination of atmosphere and imaging system in the case when the source is partially coherent, and can be represented by the quasi-stationary model employed by Carter and Wolf, ¹⁰ and Leader. ¹¹ The limiting case when the source consists of 2 point sources with random phase relationship has been studied by Miller and Korff. ¹²

⁽Received for publication 29 March 1979)

Due to the number of references to be included as footnotes on this page, the reader is referred to the list of references, page 15.

2. ANALYTICAL FORMALISM

In the Labeyrie^{6, 7} procedure a series of short exposure photographs of a star are taken and then successively projected, in the conventional manner, by a laser onto a second piece of film. This leads to an evaluation of the ensemble average of the modulus squared of the Fourier transform of the irradiance, and gives finer detail than conventional seeing calculations predict should be resolvable in the presence of atmospheric turbulence.

In order to discuss the aforementioned method quantitatively, let us refer to Figure 1. If the field distribution of the source is denoted by $u_0(\underline{\rho}_1)$, the field in the image plane, where film is located is,

$$u_{f}(\underline{\rho}) = \frac{e^{-ik(L+x)}}{\lambda^{2} Lx} \int_{-\infty}^{\infty} d^{2} \rho_{1} u_{o}(\underline{\rho}_{1}) M (\underline{\rho}_{1},\underline{\rho})$$
 (1)

where

$$M(\underline{\rho}_1,\underline{\rho}) = \iint_{-\infty}^{\infty} d^2 \rho_2 T(\underline{\rho}_2) \exp \left\{ i k \underline{\rho}_2 \cdot \left(\frac{\underline{\rho}_1}{x} + \frac{\underline{\rho}}{L} \right) + \psi(\underline{\rho}_2,\underline{\rho}_1) \right\} . \quad (2)$$

In writing Eq. (1) we have assumed that the film is in the Fraunhofer zone of the source, defined $T(\underline{\rho}_2)$ as the transmissivity of the aperture and $k=2\pi/\lambda$ as the signal wavenumber. Also $\psi(\underline{\rho}_2,\underline{\rho}_1)$ is the additional complex phase, due to atmospheric turbulence, of a spherical wave propagating from the point $(x,\underline{\rho}_1)$ on the source to the point $(0,\underline{\rho}_2)$ in the aperture. The short-exposure transparency on the film is proportional to u_1^{μ} . N such short exposures are made, with the time interval between successive exposures greater than the atmospheric coherence time, so that we have N statistically independent short exposure photographs. If a photographic plate is then placed at x=-L, and these exposures successively projected onto it, it is found that the transparency on the plate is proportional to $(|\hat{I}_f(k\underline{\rho}/L)|^2)$, where

^{*}If the film is in the Fresnel zone, we simply replace $u_{\ell}(\underline{\rho})$ by $u_{\ell}(\underline{\rho})$ exp $(i k \rho^2/2L)$, and $u_{0}(\underline{\rho}_{1})$ by $u_{0}(\underline{\rho}_{1})$ exp $(-i k \rho_{1}^2/2x)$.

^{**}By short exposure we mean short compared with the coherence time of the atmosphere.

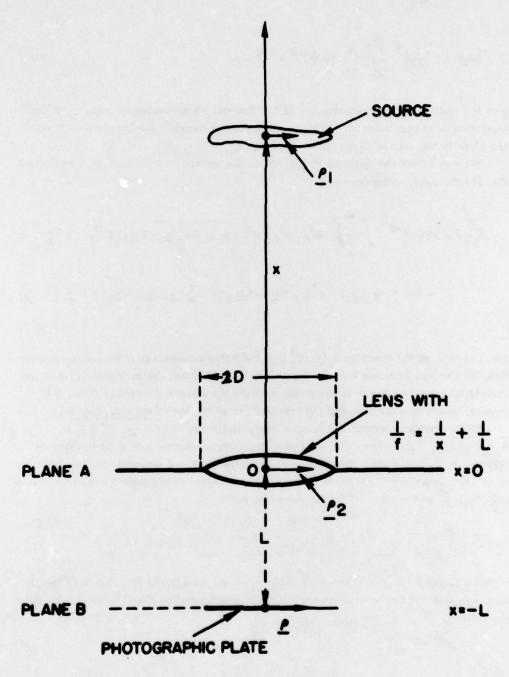


Figure 1. Geometry Assumed for the Imaging System

$$\hat{I}_{\underline{f}}(\underline{\omega}) = \left(\frac{1}{2\pi}\right)^2 \int_{-\infty}^{\infty} d^2\rho |u_{\underline{f}}(\underline{\rho})|^2 e^{i\underline{\omega}\cdot\underline{\rho}} , \qquad (3)$$

 $\underline{\omega}$ is the radian spatial frequency, and $\langle \ \rangle$ denotes an ensemble average over the statistics of the turbulence. This average occurs because the transparency on the plate is the sum of N $\gg 1$ short exposures.

We can relate the quantity in Eq. (3) to the source distribution by substituting Eq. (1) for $u_f(\underline{\rho})$. The result is

$$\hat{\mathbf{I}}_{\mathbf{f}}(\underline{\omega}) = (2\pi\lambda_{\mathbf{x}})^{-2} \int \cdots \int_{-\infty}^{\infty} d^{2}\rho_{1} d^{2}\rho_{2} d^{2}\rho_{3} \overline{\mathbf{u}_{0}(\underline{\rho}_{1}) \mathbf{u}_{0}^{*}(\underline{\rho}_{3})} T(\underline{\rho}_{2}) T^{*}\left(\underline{\rho}_{2} + \frac{\underline{\omega} L}{k}\right)$$

$$\cdot \exp\left\{\psi(\underline{\rho}_{2},\underline{\rho}_{1}) + \psi^{*}(\underline{\rho}_{2} + \underline{\omega} L/k,\underline{\rho}_{3}) + i \frac{k}{x}\underline{\rho}_{2} \cdot (\underline{\rho}_{1} - \underline{\rho}_{3}) - i \frac{L}{x}\underline{\omega} \cdot \underline{\rho}_{3}\right\}$$
(4)

The overbar on the quantity $u_0(\rho_1)u_0^*(\rho_3)$ indicates an average over source statistics, and arises because it has been tacitly assumed that the exposure time of the individual speckle pattern is much longer than the source coherence time, but of course, much shorter than the coherence time of the turbulent atmosphere.

For a spatially incoherent source one usually assumes $u_o(\varrho_1)u_o^*(\varrho_3) = A_c I_s(\varrho_1) \delta(\varrho_1 - \varrho_3)$ where $\delta(\ldots)$ is the Dirac delta function and I_s is the source irradiance distribution. However, for partially coherent sources this assumption is invalid, and instead we shall employ the quasi-stationary model used by Carter and Wolf, 10 and others. That is, we shall write

$$\overline{u_o(\varrho_1)u_o^*(\varrho_3)} \approx I_s\left(\frac{\varrho_1 + \varrho_3}{2}\right) g(\varrho_1 - \varrho_3)$$
(5)

where g is the correlation function of the source. In writing Eq. (5), it is tacitly assumed that the source coherence length is much smaller than the total size of the source.

We now use Eq. (5) in Eq. (4), define sum and difference coordinates $\underline{\xi} = \underline{\rho}_1 - \underline{\rho}_3$, $\underline{\eta} = (\underline{\rho}_1 + \underline{\rho}_3)/2$, etc., and then perform the ensemble average over the turbulence statistics, assuming that the source lies wholly within an isoplanatic turbulence patch, so that $\psi(\underline{\rho},\underline{\rho}') \simeq \psi(\rho,0)$. The result is

$$\langle | I_{\mathbf{f}}(\underline{\omega}) |^2 \rangle = H(\underline{\omega}) \left| \hat{I}_{\mathbf{s}} \left(\underline{\omega} \cdot \underline{\mathbf{L}} \right) \right|^2 ,$$
 (6)

where

$$\hat{I}_{\mathbf{s}}(\underline{\Omega}) = (2\pi)^{-2} \iint_{-\infty}^{\infty} d^2 \mathbf{v} \, \mathbf{I}_{\mathbf{s}}(\underline{\mathbf{v}}) \, \exp\left(-i\underline{\Omega} \cdot \underline{\mathbf{v}}\right) . \tag{7}$$

Therefore, the modulus squared of the Fourier transform of the source distribution is linearly related to the measured quantity, $\langle |I_f|^2 \rangle$. Also in Eq. (6), we have defined

$$H(\underline{\omega}) = (\lambda x)^{-4} \int_{-\infty}^{\infty} d^2 \gamma K_0(\underline{\omega}, \underline{\gamma}) \exp \left\{ -D_1 \left(\underline{\omega} \frac{L}{k}, 0 \right) - D_1(\underline{\gamma}, 0) + \frac{1}{2} D_1 \left(\underline{\gamma} - \underline{\omega} \frac{L}{k}, 0 \right) + \frac{1}{2} D_1 \left(\underline{\gamma} + \underline{\omega} \frac{L}{k}, 0 \right) \right\} , \qquad (8)$$

where

$$K_{O}(\underline{\omega},\underline{\gamma}) = \iint_{-\infty}^{\infty} d^{2}\tau \ T(\underline{\tau} + \underline{\gamma}/2) \ T^{*}(\underline{\tau} + \underline{\gamma}/2 + \underline{\omega} L/k)$$

$$\cdot \ T^{*}(\underline{\tau} - \underline{\gamma}/2) \ T(\underline{\tau} - \underline{\gamma}/2 + \underline{\omega} L/k) \ G(\underline{\tau},\underline{\gamma},\underline{\omega}) \ G^{*}(\underline{\tau},-\underline{\gamma},\underline{\omega}) \ , \tag{9}$$

^{*}The derivation of the average,

 $[\]langle \exp[\psi(\underline{\rho}_2,\underline{\rho}_1) + \psi^*(\underline{\rho}_2 + \underline{\omega} L/k,\underline{\rho}_1) + \psi^*(\underline{\rho}_5,\underline{\rho}_4) + \psi(\underline{\rho}_5 + \underline{\omega} L/k,\underline{\rho}_4)] \rangle$ over the statistics of the turbulence is given by Eq. (34) of R. Fante, "Some results on the imaging of incoherent sources through turbulence," J. Opt. Soc. Am. 66, 574-580 (1976).

and

$$G(\underline{\tau},\underline{\gamma},\underline{\omega}) = \iint_{-\infty}^{\infty} d^2\xi \ g(\underline{\xi}) \exp \left\{ i \frac{k}{x} \underline{\xi} \cdot (\underline{\tau} + \underline{\gamma}/2 + \underline{\omega} L/2k) \right\} . \tag{10}$$

The structure function D₁ of the atmospheric turbulence is given by

$$D_1(\underline{\beta}, 0) \simeq 2 |\beta/r_0|^{5/3}$$
 (11)

and the atmospheric coherence length, ro, is defined as

$$r_0 = \left[1.46 \text{ k}^2 \int_0^x \left(\frac{x-x'}{x}\right)^{5/3} C_n^2(x') dx'\right]^{-3/5}$$
, (12)

where $C_n^2(x^i)$ is the index-of-refraction structure constant of the atmosphere.

The result in Eq. (6) is of the same form as previous results obtained for a spatially incoherent source, but differs in the definition of $K_0(\underline{\omega},\underline{\gamma})$. For a spatially incoherent source, so that $g(\underline{\rho}_1 - \underline{\rho}_3) = A_c \delta(\underline{\rho}_1 - \underline{\rho}_3)$ where A_c is the coherence area of the source, we find $G = A_c$, and Eqs. (6)–(10) then reduce identically to the result of Korff¹ for the spatially incoherent source.

3. APPROXIMATE EVALUATION OF TRANSFER FUNCTION, $H(\omega)$

We would now like to investigate the effect of the partial coherence on the transfer function, $H(\underline{\omega})$. In order to do this, we will assume that the source coherence function $g(\underline{\xi})$ is given by

$$g(\underline{\xi}) = \exp\left(-\frac{\xi^2}{a^2}\right) , \qquad (13)$$

where a is the source coherence length. Upon using this expression in Eq. (10), we find

$$G(\underline{\tau}, \underline{\gamma}, \underline{\omega}) = A_c \exp \left[-\left(\frac{ka}{2x}\right)^2 |\underline{\tau} + \underline{\gamma}/2 + \underline{\omega} L/2k|^2 \right],$$
 (14)

where $A_c = \pi a^2$ is the coherence area of the source.

The next step is to substitute G into Eq. (9) and evaluate $K_0(\underline{\omega},\underline{\gamma})$. For a realistic aperture, such as on a telescope, $T(\underline{\rho}_2) = 1$ for $|\underline{\rho}_2| \leq D$ and $T(\underline{\rho}_2) = 0$ for $|\underline{\rho}_2| > D$. Unfortunately, the expression for K in Eq. (9) cannot be evaluated in closed form when this expression is used for $T(\underline{\rho}_2)$. Therefore, we have been forced to approximate $T(\underline{\rho}_2)$ by the function $T(\underline{\rho}_2) = \exp(-\rho_2^2/D^2)$, with the realization that, because we are approximating the edge diffraction, our results will be valid only for radian spatial frequencies such that $|\underline{\omega}| < kD/L$. That is, setting $T(\underline{\rho}_2) = 0$ for $|\underline{\rho}_2| > D$ would give $H(\underline{\omega}) = 0$ for $|\underline{\omega}| > kD/L$; however, because we will approximate $T(\underline{\rho}_2)$ by $\exp(-\rho_2^2/D^2)$ we will obtain an expression for $H(\underline{\omega})$ which does not vanish for $|\underline{\omega}| > kD/L$. If the aforementioned approximation is used, along with Eq. (14), in Eq. (9) we find that

$$K_{O}(\underline{\omega},\underline{\gamma}) = \frac{\frac{\pi}{4} A_{C}^{2} \exp \left\{-\frac{\omega^{2} L^{2}}{k^{2} D^{2}} - \gamma^{2} \left(\frac{1}{\ell_{C}^{2}} + \frac{1}{D^{2}}\right)\right\}}{\left(\frac{1}{\ell_{C}^{2}} + \frac{1}{D^{2}}\right)},$$
(15)

where $I_c = 2^{3/2} x/(ka) = (2/\pi A_c)^{1/2} \lambda x$ is the coherence length, as measured at the receiving aperture, of the field radiated by a coherence patch of radius a on the source.

We next investigate the behavior of the function

$$C(\underline{\omega},\underline{\gamma}) = \exp\left\{-D_{1}(\underline{\omega}L/k,0) - D_{1}(\underline{\gamma},0) + \frac{1}{2}D_{1}(\underline{\gamma} - \underline{\omega}L/k,0) + \frac{1}{2}D_{1}(\underline{\gamma} + \underline{\omega}L/k,0)\right\}.$$
(16)

It is found that for $|\omega| \ll kr_0/L$, this function can be approximated by unity. However, the more interesting case occurs ** when $|\omega| \gg kr_0/L$. In this limit, $C(\underline{\omega}, \underline{\gamma})$ can be approximated by

$$C(\underline{\omega},\underline{\gamma}) \simeq \exp \left\{-2\left|\underline{\gamma}/r_{o}\right|^{5/3}\right\} . \tag{17}$$

The result in Eq. (17) is inconvenient for analytical purposes; consequently, we shall approximate the exponent in Eq. (17) by a quadratic function, so that

^{*}The evaluation can be performed in the limit when $G(\xi) = A_c$.

^{**}We are assuming that $r_0 < D$. For $r_0 \gg D$, the atmospheric turbulence has an insignificant effect on the imaging.

$$C(\underline{\omega}, \underline{\gamma}) \simeq \exp \left\{-2.296 \left|\underline{\gamma}/r_0\right|^2\right\}$$
 (18)

The function in Eq. (18) is such that C equals e^{-1} at the same value of $|\underline{\gamma}|$ as does the function in Eq. (17).

If we now use Eqs. (15) and (18) in Eq. (8), we can calculate the transfer function $H(\underline{\omega})$. For values of $|\underline{\omega}|$ such that $|\underline{\omega}| \gg kr_o/L$, the result is *

$$H(\underline{\omega}) = \frac{K \exp(-\omega^2 L^2 / k^2 D^2)}{\left[1 + \left(\frac{D}{t_c}\right)^2\right] \left[1 + \left(\frac{D}{t_c}\right)^2 + 2.296 \left(\frac{D}{r_o}\right)^2\right]},$$
 (19)

where

$$K = 2.467 \left(\frac{D}{x}\right)^4 \left(\frac{A_c^2}{\lambda^4}\right) = \left(\frac{D}{t_c}\right)^4 . \tag{20}$$

Because of our approximation for $T(\varrho_2)$, the result in Eq. (19) can be applied to realistic apertures only for spatial frequencies such that $|\omega| < kD/L$. In the limit when $r_0 \ll D$ and the source is incoherent, so that $t_c \to \infty$, Eq. (19) reduces to the high-spatial frequency approximation obtained by Korff. ¹

For values of $[\omega]$ such that $[\omega] \ll kr_0/L$ the evaluation of Eq. (8) gives

$$H(\underline{\omega}) = \frac{K}{\left[1 + \left(\frac{D}{t_c}\right)^2\right]^2} \qquad (21)$$

A qualitative plot of $H(\omega)$ is shown in Figure 2, for the limits when $r_0 \ll D$ and $r_0 \gg D$. In this latter case, of course, the turbulent atmosphere does not affect the imaging.

^{*}Note that $H(\omega)$ is not normalized to unity at ω =0, as is often done.

^{**}Strictly speaking t_c never really becomes infinite, because $a \ge \lambda$. Therefore, $t_c + 2^{1/2} \pi^{-1} x$.

Because r_0 is assumed to be less than D, the assumption that $|\omega| \ll kr_0/L$ implies that $|\omega| L/kD| \ll 1$. Consequently, in Eq. (21) we have approximated $\exp{(-\omega^2 L^2/k^2D^2)}$ by unity.

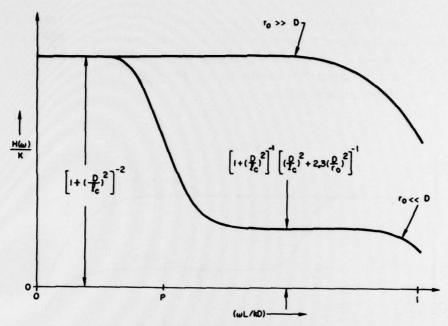


Figure 2. Qualitative Plot of $H(\underline{\omega})$. The point P corresponds to $\underline{\omega} \simeq kr_0/L$

4. DISCUSSION

From Figure 2, we observe that the amplitude of $H(\underline{\omega})$ at small spatial frequencies is determined by the size of D/ℓ_c . For $\ell_c \gg D$ we get the usual Labeyrie result, but when $\ell_c \ll D$ the result in Eq. (21) becomes $H(\underline{\omega}) \to 1$.

It is also interesting to observe the nature of the high-spatial-frequency plateau in $H(\underline{\omega})$ for the case when $r_0 \ll D$. We will not discuss the case when $r_0 \gg D$ because in that limit atmospheric turbulence does not affect the image. If $r_0 \ll D$ but $I_c \gg D$, we get the previous result of Korff; however, if $r_0 \ll D$ and $I_c \ll D$ we find, for $|\underline{\omega}| > kr_0/L$

$$H(\omega) \simeq \frac{\exp(-\omega^2 L^2/k^2 D^2)}{1 + 2.296 \left(\frac{l_c}{r_o}\right)^2}$$
 (22)

From Eq. (22) we see that if $t_c \ll r_o$, $H(\underline{\omega}) \to \exp{(-\omega^2 L^2/k^2 D^2)}$, and the high-frequency transfer function approaches that for a coherent source. However, when t_c is of order or greater than r_o the amplitude of $H(\omega)$ differs from $\exp{(-\omega^2 L^2/k^2 D^2)}$. Qualitative results for $H(\underline{\omega})$ in the limit when both $t_c \ll D$ and $r_o \ll D$ are shown in Figure 3.

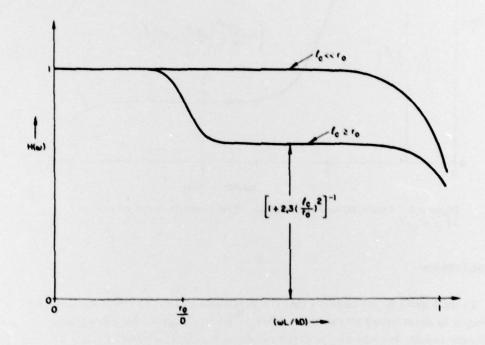


Figure 3. Qualitative Plot of $H(\underline{\omega})$ for the Case When Both $t_{_{\rm C}}\ll {\rm D}$ and ${\rm r}_{_{\rm O}}\ll {\rm D}$

References

- Korff, D. (1973) Analysis of a method for obtaining near-diffraction-limited information in the presence of atmospheric turbulence, J. Opt. Soc. Am. 63:971-980.
- Korff, D., Dryden, G., and Miller, M. (1972) Information retrieval for atmospheric induced speckle patterns, Optics Commun. 5:187-192.
- Karo, D., and Schneiderman, A. (1976) Speckle interferometry lens-atmosphere MTF measurements, J. Opt. Soc. Am. 66:1252-1256.
- Karo, D., and Schneiderman, A. (1978) Speckle interferometry at finite spectral bandwidths and exposure times, J. Opt. Soc. Am. 68:480-485.
- Shapiro, J. (1978) Laser propagation in the atmosphere, in <u>Topics in Applied Physics</u>, Vol. 25 (J. Strohbehn, Editor) Springer-Verlag, <u>Berlin</u>.
- Labeyrie, A. (1970) Attainment of diffraction limited resolution in large telescopes by Fourier analyzing speckle patterns in star images, Astron. Astrophys. 6:85-87.
- Gezari, D., Labeyrie, A., and Stachnik, R. (1972) Speckle interferometry: diffraction limited measurement of nine stars with the 200 inch telescope, Astrophys. J. 173:L1-L5.
- Aime, C. (1974) Measurement of the average squared modulus of the atmosphere-lens modulation transfer function, J. Opt. Soc. Am. 64: 1129-1132.
- Aime, C., Ricord, G., Roddier, C., and Lago, G. (1978) Changes in the atmospheric-lens modulation transfer function used for calibration in solar speckle interferometry, J. Opt. Soc. Am. 68:1063-1066.
- Carter, W., and Wolf, E. (1977) Coherence and radiometry with quasihomogeneous planar sources, J. Opt. Soc. Am. 67:785-796.
- Leader, J.C. (1978) Far-zone criteria for quasi-homogeneous partially coherent sources, J. Opt. Soc. Am. 68:1332-1338.
- Miller, M., and Korff, D. (1974) Speckle interferometry with partially coherent light, J. Opt. Soc. Am. 64:155-159.

MISSION of Rome Air Development Center

acture of the state of the stat

RADC plans and executes research, development, test and selected acquisition programs in support of Command, Control Communications and Intelligence (C³I) activities. Technical and engineering support within areas of technical competence is provided to ESD Program Offices (POs) and other ESD elements. The principal technical mission areas are communications, electromagnetic guidance and control, surveillance of ground and aerospace objects, intelligence data collection and handling, information system technology, ionospheric propagation, solid state sciences, microwave physics and electronic reliability, maintainability and compatibility.